

PAPER • OPEN ACCESS

Improved algorithm for minimum zone of roundness error evaluation using alternating exchange approach

To cite this article: Alhadi Khilil *et al* 2022 *Meas. Sci. Technol.* **33** 045003

View the [article online](#) for updates and enhancements.

You may also like

- [Improved evaluation of minimum zone roundness using an optimal solution guidance algorithm](#)
Jingzhi Huang, Runze Yang, Haiqiao Ge et al.
- [An iterative neighborhood search approach for minimum zone circularity evaluation from coordinate measuring machine data](#)
Changcai Cui, Wei Fan and Fugui Huang
- [Improved evaluation of minimum zone roundness by integrating bidirectional search of unequal probability and offset mechanisms](#)
Jingzhi Huang, Xiangzhang Chao, Lin Jiang et al.

Improved algorithm for minimum zone of roundness error evaluation using alternating exchange approach

Alhadi Khilil , Zhanqun Shi*, Abubakar Umar  and BoTong Ma

School of Mechanical Engineering, Hebei University of Technology, Tianjin 300401, People's Republic of China

E-mail: z_shi@hebut.edu.cn

Received 30 June 2021, revised 8 November 2021

Accepted for publication 7 December 2021

Published 7 January 2022



CrossMark

Abstract

Based on computational geometry techniques, an improved algorithm for the minimum zone of roundness error evaluation using an alternating exchange method is presented. A minimum zone fitting function was created to enhance the roundness error evaluation. The function uses three candidate points to determine the initial solution: the expected centre, the mean circle radius, and the corresponding zone half-width. The best solution function is designed to use the initial solution as the input to determine the optimum solution for the minimum zone circle (MZC). The proposed algorithm was validated using data available in the literature. The roundness error evaluation comparison results demonstrate that the proposed method accurately detects both the centre error magnitude and MZC and overcomes the insufficiency of using selected colinear points for four selected points.

Keywords: roundness error evaluation, minimum zone circle, alternating exchange algorithm

(Some figures may appear in colour only in the online journal)

1. Introduction

The roundness error is a fundamental criterion in quality inspection for validating produced parts. This error has been specified by the American National Standards Institute (ANSI) under dimensioning and tolerance standards [1, 2], as well as by the International Organization for Standardization (ISO) under their geometrical product specifications [3, 4]. Owing to the complexity and uncertainty of machining processes, soft computing techniques are preferred for evaluating the roundness error [5]. These techniques are primarily classified into

two groups: algebraic-based techniques and computational geometry-based techniques [6]. The most commonly used methods for the evaluation of roundness error are the least-square circle method, minimum zone circle (MZC) method, minimum circumscribed circle (MCC) method, and maximum inscribed circle (MIC) method [7]. Among these, only the MZC has been confirmed by ANSI and ISO. Although the MZC is extensively used for the evaluation of roundness errors, there is no specific procedure for establishing a reference feature [8]. Therefore, researchers have focused on improving the accuracy of roundness error evaluation.

In recent years, numerous studies have addressed the MZC evaluation of roundness errors. Different methods have been used to solve linear and nonlinear MZC problems. Based on nonlinear optimisation, a genetic algorithm was proposed by Wen *et al* [9]. However, although this technique is robust, it has only been applied to small samples. For cases with a significant number of sample points, a fast genetic algorithm

* Author to whom any correspondence should be addressed.



Original content from this work may be used under the terms of the [Creative Commons Attribution 4.0 licence](https://creativecommons.org/licenses/by/4.0/). Any further distribution of this work must maintain attribution to the author(s) and the title of the work, journal citation and DOI.

was implemented. The applied genetic parameters include population size, crossover, mutation, stop condition, and search space. The use of ideal genetic parameters improves the feasibility of a solution while reducing the computing time [10]. By contrast, Du *et al* [11] introduced a particle swarm algorithm that can avoid becoming trapped in the local minimum of the optimisation by changing the weight. However, the computation time is a key factor in metaheuristic methods. Rossi *et al* [12] presented an optimal sampling strategy that provided sufficient accuracy with an appropriate processing time. Moreover, computational geometry methods have also been widely used to evaluate the roundness error. Lei *et al* [13] introduced a roundness error evaluation method based on a polar coordinate transform algorithm (PCTA). Similarly, Ben *et al* [14] presented a rapid precision evaluation of the roundness error in polar coordinates. However, the accuracy of this method depends on the number of mesh points, which is expensive in some cases. In another study, a four-point intersection principle and bisection method were introduced to evaluate the MZCs [15]. This method focuses on improving the selection of the initial points. The chord intersection relationship is also used to accurately determine the centre coordinates of the concentric circles [16]. The roundness error has also been evaluated using other approaches, such as integrating the bidirectional search of unequal probability and offset mechanisms [17], hybrid global search [8], selection of four points [18], worst-case analysis [19], the concept of convex hulls, and the newly proposed equi-angular diagrams [20]. Based on a selected point dataset, Muralikrishnan *et al* [21] discussed the implementation of the alternating exchange algorithm. This method determines the MZC using a set of four selected points. According to [22], this method can fail to achieve the best approximation if the four points are collinear or are at the vertices of a (convex) quadrilateral with a pair of opposite sides parallel.

This paper proposes an algorithm that utilises a set of three selected points to enhance the positioning of the MZC centre coordinate to create the best approximation and thus avoid failures caused by collinear selected points. However, the direct mathematical calculation for the MZC defined by three points does not guarantee the best solution. Hence, to obtain the best solution, an improved alternating exchange algorithm with a realistic pre-construct geometry was developed.

2. Methodology

2.1. Principle of MZC

According to the definition of MZC, the problem requires the identification of two concentric circles that confine all the dataset points with a minimal difference in their radii [3], which is given by

$$\left. \begin{aligned} r_1 &= \sqrt{(x_1 - a)^2 + (y_1 - b)^2} \\ r_2 &= \sqrt{(x_2 - a)^2 + (y_2 - b)^2} \end{aligned} \right\} \quad (1)$$

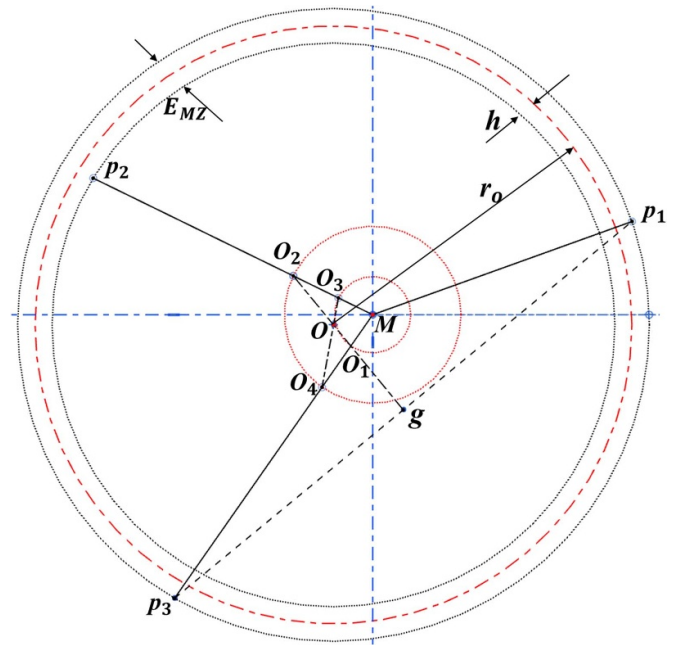


Figure 1. Minimum zone fitting function parameters.

where r_1 and r_2 represent the outer and inner minimum zone radii, respectively; (a, b) , the MZ coordinate centre; and (x_1, y_1) , (x_2, y_2) , the furthest boundary points.

The roundness error of the MZC is given as follows:

$$E_{MZ} = |r_1 - r_2|. \quad (2)$$

2.2. Improved exchange algorithm

The algorithm intends to specify the centre coordinate of the MZCs $O(a, b)$, with respect to the measurement origin M , the mean radius r_0 , and the current zone half-width h . The proposed algorithm relies on the geometry interception properties, as shown in figure 1. It takes three selected points from the measured dataset as inputs p_1, p_2, p_3 , which are denoted as the critical points and are selected randomly for the first iteration. Two concentric circles will be constructed from a temporary specified centre $O(a, b)$; current zone half-width h will be used to verify whether any points are outside the current zone; and the two concentric circles that confine all the datasets will represent the minimum zone error. The basic consideration comes from the exchange algorithm, and it proves that for selected set points p_1, p_3, p_3 no two consequent points should be on the same circle, which allows us to say that (p_1, p_3) specifies one circle (outer boundary), and p_2 specifies the other circle (inner boundary). In addition, by the theorem of the circle, the best centre must be located somewhere on the $\overline{p_1 p_3}$ bisector. According to [13], the specified minimum zone coordinate centre point of the MIC, MCC, and MZC are located in a small zone area around the measurement origin M .

2.2.1. Small zone specification. To identify the proposed small zone, we assume p_1, p_3 to be in the same circle (outer boundary) and take $\overline{p_1 p_3}$ as a chord in this circle, with the

constructed bisector in g . We construct two small circles referenced in M using the intersection points O_1, O_2 . The first circle is constructed with a radius $\overline{MO_1}$ and the second circle with a radius $\overline{MO_2}$. Then, we consider the quadrilateral shape O_1, O_2, O_3, O_4 as the proposed small zone.

2.2.2. Minimum zone fitting function. According to the alternating exchange algorithm, the function is intended to search for the furthest inner and outer points p_1, p_2, p_3 ; this function helps obtain the MZC error by updating these points in each iteration. Since the exchange algorithm is based on the mean radius r_0 and minimum zone half-width between the two concentric circles h ; then, from the assumed small zone, as shown in figure 1, the interception point of the $\overline{p_1p_3}$ bisector and the angle P_2, M, P_3 bisector can be obtained as a good approximation of the concentric centre point $O(a, b)$. Thus, to achieve the centre of two concentric MZCs, the chords $(\overline{O_1O_2}, \overline{O_3O_4})$ interception of the quadrilateral shape $O_1O_2O_3O_4$ is considered as the MZC centre $(O(a, b))$ for specifically selected points in each iteration.

Thus, from the selected critical points p_1, p_2, p_3 , with it is corresponding temporarily obtained centre $O(a, b)$, we rewrite equation (1) as follows:

$$\left. \begin{aligned} r_1 &= \sqrt{(x(p_1) - a)^2 + (y(p_1) - b)^2} \\ r_2 &= \sqrt{(x(p_2) - a)^2 + (y(p_2) - b)^2} \\ r_3 &= \sqrt{(x(p_3) - a)^2 + (y(p_3) - b)^2} \end{aligned} \right\}. \quad (3)$$

The specified mean radius r_0 is given as follows:

$$r_0 = \frac{r_1 + r_2}{2}. \quad (4)$$

Further, the minimum zone half-width between the two concentric circles, h , is given as follows:

$$h = \frac{r_1 - r_2}{2}. \quad (5)$$

Practically, the obtained centre $O(a, b)$ of the minimum zone for particularly critical points is located in a triangular sector area p_1Mp_2 when $p_1 > p_3$ and

$$\text{sgn}(x_2) = \text{sgn}(a_2).$$

Alternatively, it will be located in a triangular sector area p_3Mp_2 when $p_3 > p_1$ and

$$\text{sgn}(x_2) = \text{sgn}(a_2).$$

Otherwise, we invert the signs of $O_3(a_3, b_3)$ for calculating the centre $O(a, b)$. This is because the incommensurate signs of x_2 and a_2 indicate that the intersection point O_2 between $\overline{p_1p_3}$ bisector and $\overline{Mp_2}$ is on the extension of $\overline{Mp_2}$.

A particular condition should also be noted. Consider $Mp_1 = Mp_3$ indicates that the $\overline{p_1p_3}$ bisector is passing through M and intercept of Mp_2 also on M . In this case, geometrically, $O_1 = O_2 = O_3 = O_4 = M$. However, to allow the algorithm

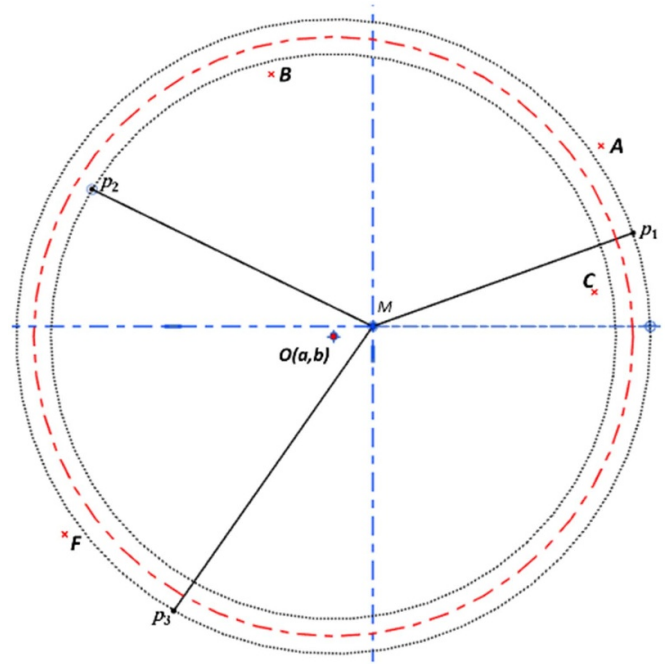


Figure 2. Alternating exchange rule.

to handle this situation, we add the following condition in the minimum zone fitting function:

$$\text{if } O_1(a_1, b_1) = M$$

$$\text{then } O(a, b) = M.$$

2.2.3. Alternating exchange rule. The alternating exchange rule [21] is used to replace the undesirable point in each iteration till we reach the desired points.

The fitting function output was used to determine the minimum zone boundaries. The exchange algorithm checks any point out of the obtained boundaries, which are denoted as the outlier points, by calculating the deviations (dev) between the mean radius and the distance from (a, b) to (x_i, y_i)

$$\text{dev} = r_0 - \sqrt{(x_i - a)^2 + (y_i - b)^2} \quad (6)$$

$$i = 1 \sim n,$$

where n is the number of measured data.

If $h > |dev_i|$, it indicates that there is no outlier point, and the result is accepted as the initial solution. If $h < |dev_i|$, then the specific point (i) is the outlier point, and we apply the alternating rule to replace the outlier point with one of the critical points. As shown in figure 2, the current minimum zone boundaries were defined by critical points (p_1, p_2, p_3) and were ordered anticlockwise starting from the positive x axis. To apply the alternating rule, for example, if we consider A to be an outlier point because A lies outside the outer boundary, we can only consider the replacement of $(p_1$ or $p_3)$; in this case,

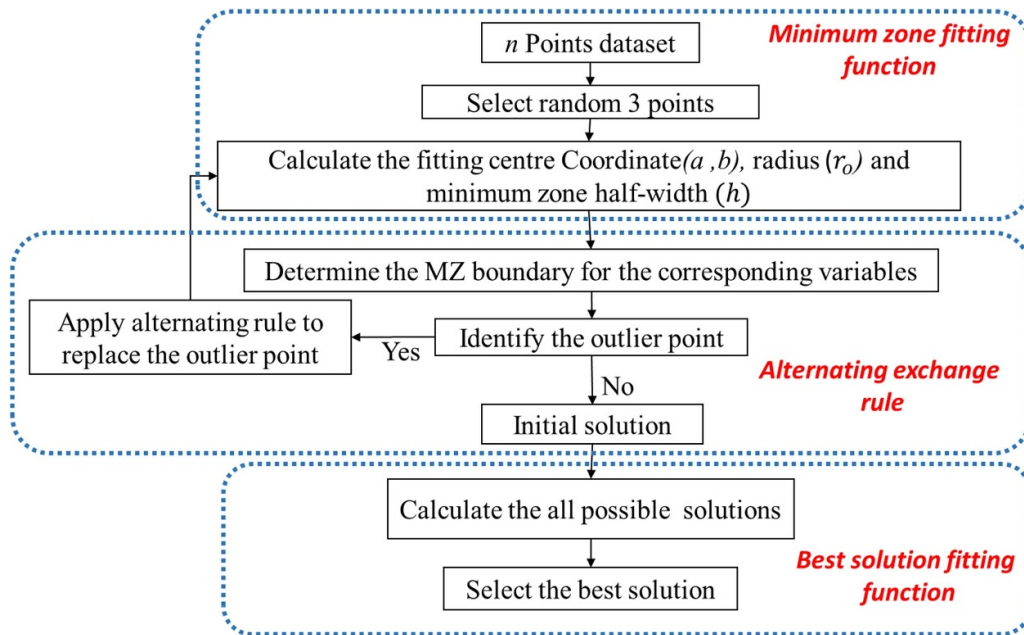


Figure 3. Proposed algorithm structure.

it will be replaced with p_1 . Similarly, consider different situations for the outliers. If B is an outlier point, we can replace it with p_2 . If C is an outlier point, we can replace it with p_3 and re-order the points. If F is an outlier point, we can replace it with p_3 . Muralikrishnan and Raja have discussed in detail the alternating exchange algorithm [21]. As illustrated in the flow chart in figure 3, if there is no outlier point, we assume the result to be an appropriate initial solution.

2.2.4. Best solution fitting function. The best solution fitting function uses the initial solution obtained from the minimum zone fitting function to obtain an optimum solution. It also uses a simple alternating exchange rule to calculate all the possible solutions that can be obtained by replacing $p_i, i = 1 \sim (n - 3)$ with the current critical points (p_1, p_2, p_3) . The function retains two points from the current critical points and replaces the third point. For $p_i < p_2$, we take $p_i = p_1$, while for $p_i > p_2$, we take $p_i = p_3$, then collect all the possible solutions. Among these solutions, the function selects the minimal h and then use its corresponding critical points to calculate the optimum solution as follows:

- The $\overline{p_1 p_3}$ bisector contains the best minimum zone centre; further, from the proposed small zone, the line segment $\overline{O_1 O_2}$ is considered to be the best search line of the MZC centre.
- $\overline{O_1 O_2}$, which is extremely small, is divided to produce m centre points; increasing the value of m helps precisely cover the line segment.
- Equations (4) and (5) and m number of coordinate evaluation centres are used to obtain r_o and h ; the minimum constructed concentric circles division is adopted as the best minimum zone error solution.

The structure of the improved MZC algorithm for roundness error evaluation is shown in figure 3. It consists of a set of algorithms developed using MATLAB software. The first step is to select three random points representing the first iteration parameters. The second step involves using the developed fitting function to obtain the parameters of the minimum zone error evaluation. And then identify the inner and outer minimum zone boundaries. The third step is to use an alternating exchange principle to examine the validity of the current boundaries. If it confines all the datasets, then we regard the result as being the initial solution. Otherwise, we apply the alternating rule to replace one of the three currently selected points with the farthest point until we obtain a valid initial solution. The fourth step is to use a constructed best solution fitting function to calculate all the possible solutions from the corresponding dataset and select the best solution, representing the intended MZC of the roundness error.

3. Algorithm verification using practical datasets

Three different datasets were used to validate the proposed algorithm. The first dataset was taken from literature [11] and uses the PCTA. The second dataset originated in literature [23]. The third dataset was produced from a quality-control measurement system. This is currently under development, and the system and its simulation are described in [24].

4. Results

The results obtained from the adopted data information are used as benchmarks to track the performance of the proposed algorithm. As summarised in table 1, the accuracy of the MZ error evaluation depends on equally dividing m . Increasing the number of divisions is guaranteed to improve the accuracy of

Table 1. Effect of dividing quantity m .

Divide points MZ parameters	$m = 10$			$m = 30$			$m = 50$		
	Magnitude (mm)	Angle (rad)	MZ error (mm)	Magnitude (mm)	Angle (rad)	MZ error (mm)	Magnitude (mm)	Angle (rad)	MZ error (mm)
Data set 1	0.003 25	3.5340	0.0280	0.002 25	4.9465	0.0275	0.002 21	5.1198	0.0274
Data set 2	0.011 039	0.5267	0.008 46	0.012 170	0.5130	0.008 38	0.012 40	0.5105	0.008 36
Data set 3	0.004 973	0.9077	0.025 19	0.005 074	0.8404	0.0248 60	0.005 098	0.827 29	0.0247 94
Divide points MZ parameters	$m = 80$			$m = 100$			$m = 120$		
	Magnitude (mm)	Angle (rad)	MZ error (mm)	Magnitude (mm)	Angle (rad)	MZ error (mm)	Magnitude (mm)	Angle (rad)	MZ error (mm)
Data set 1	0.002 27	5.3796	0.0273	0.002 27	5.3796	0.0272	0.002 27	5.3796	0.0272
Data set 2	0.012 73	0.5070	0.008 34	0.0127	0.5070	0.008 34	0.0127	0.5070	0.008 34
Data set 3	0.005 111	0.8111	0.02476	0.005 115	0.8175	0.02474	0.005 118	0.815 91	0.0247 35

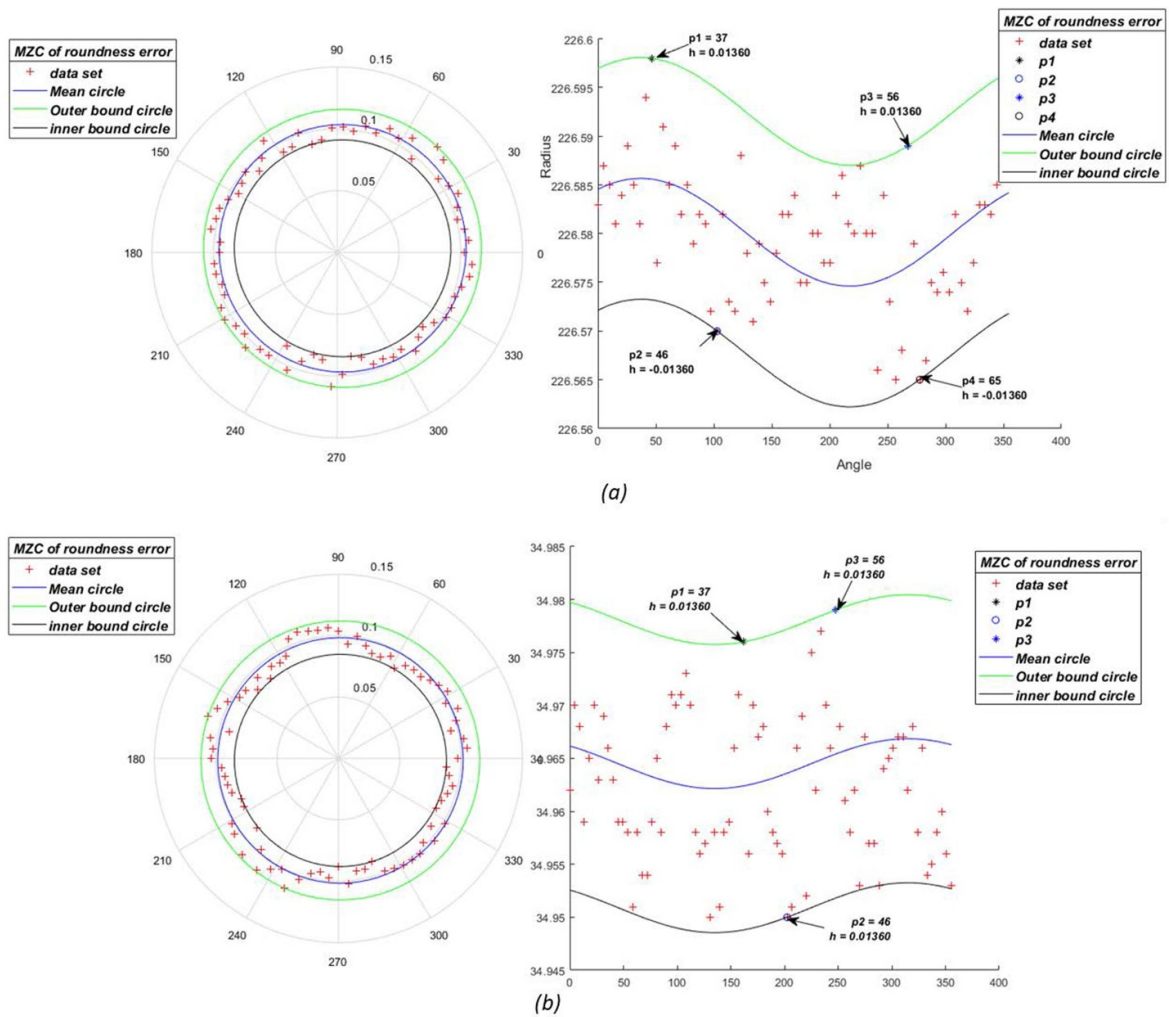


Figure 4. Results for (a) alternating exchange algorithm set, and (b) proposed algorithm using the first data set.

Table 2. Comparison for first dataset.

Method	Coordinate centre		MZ roundness error (mm)
	Magnitude (mm)	Angle (rad)	
PCTA	0.0023	5.4766	0.0272
Exchange algorithm	0.0024	5.4978	0.0272
Present method	0.0023	5.3796	0.0272

Table 3. Comparison for second dataset.

Method	Coordinate centre		MZ roundness error (mm)
	Magnitude (mm)	Angle (rad)	
Least-square algorithm	0.00	—	0.0097
Exchange algorithm	0.0229	1.0247	0.008 359
Present method	0.0127	0.5070	0.008 343

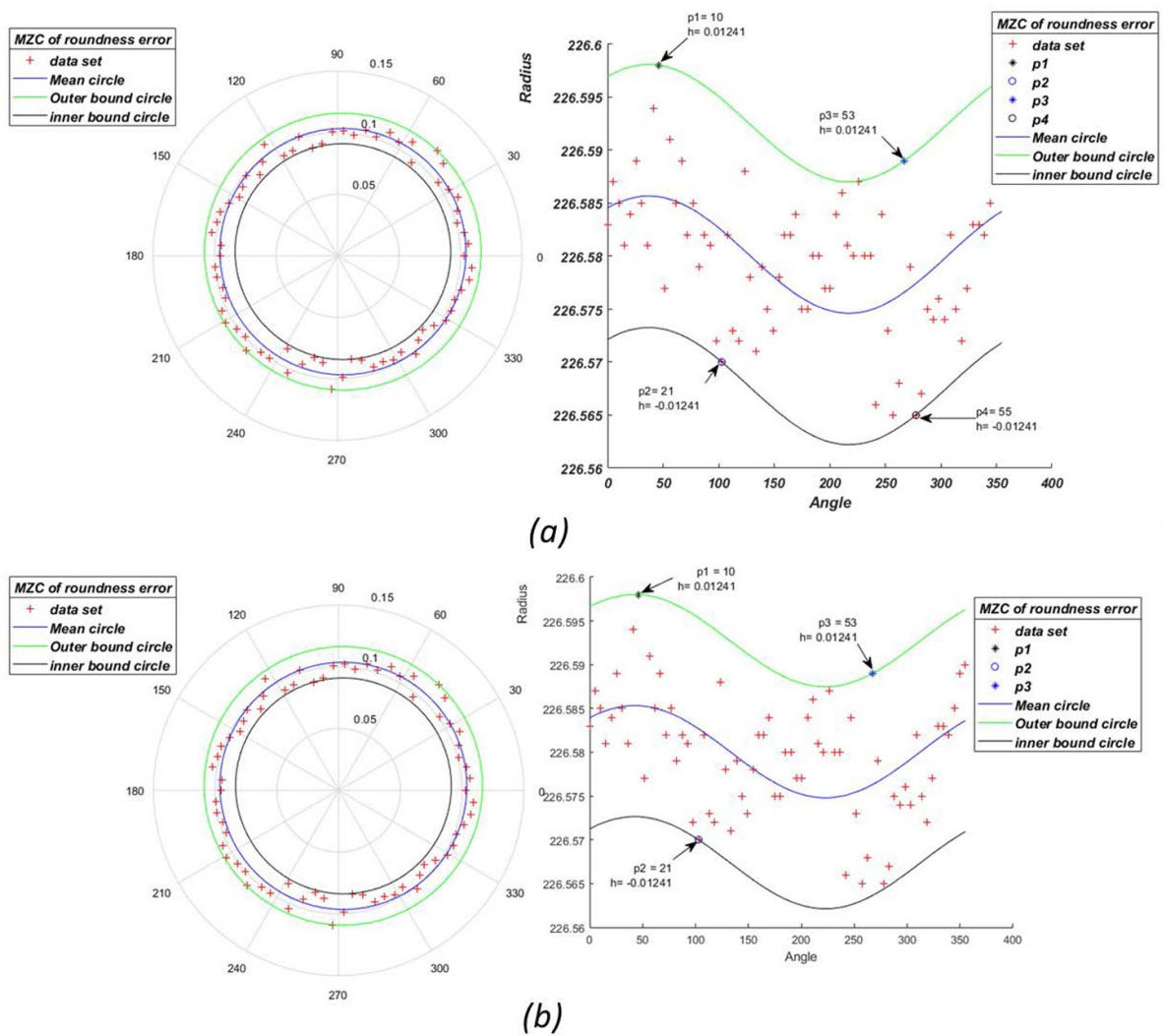


Figure 5. Results for (a) alternating exchange algorithm, and (b) proposed algorithm using the third data set.

Table 4. Comparison for third dataset.

Method	Coordinate centre		MZ roundness error (mm)
	The magnitude (mm)	Angle (rad)	
Exchange algorithm	0.005 53	0.922	0.0248
The present method	0.005 12	0.818	0.0247

the MZ roundness error evaluation. Table 1 indicates that a higher value of m does not considerably influence the results; thus, from the practical result, $80 < m < 100$ is adequate to obtain more accurate results.

The simulation results produced using the first dataset are shown in figure 4(a), where the critical points for the alternating exchange algorithm are 37, 46, 56, and 65. Figure 4(b) illustrates the results obtained with the proposed algorithm, where the critical points are 37, 46, and 56. Table 2 lists the results obtained with the proposed algorithm, where the MZC error evaluation is 0.0272 mm and the magnitude of the coordinate centre is 0.0023 mm, similar to that of the PCTA; further, the magnitude of the coordinate centre for the alternating exchange algorithm is 0.0024 mm. The proposed algorithm and PCTA method are slightly superior in terms of the centre error, although this does not affect the accuracy of the final result. The proposed algorithm provides an accurate result comparable to that obtained with PCTA and the exchange algorithm in terms of the minimum zone error and error magnitude of the coordinate centre.

The simulation results produced using the second dataset are presented in table 3. The critical points for the exchange algorithm are 7, 10, 11, and 19, while the points for the proposed algorithm are 1, 11, and 19. The calculated MZC error of the proposed algorithm is 0.008343 mm and that of the alternating exchange algorithm is 0.008359 mm. A slight variation was noted in the MZC error result. However, the magnitude of the coordinate centre eccentricity using the proposed algorithm is 0.0127 mm, while it is 0.0229 mm with the alternating exchange algorithm, pointing to the superior performance of the proposed algorithm considering the roundness error calculation.

Moreover, the simulation results obtained from the third dataset are shown in figure 5(a), where the critical points for the alternating exchange algorithm are 10, 21, 53, and 55. Figure 5(b) illustrates the results for the proposed algorithm, where the critical points are 10, 21, and 53. The results listed in table 4 indicate that the proposed algorithm performance follows similar results in structure as in the previous results. The MZC error of the proposed algorithm (0.0247 mm) is less than in the case of the alternating exchange algorithm (0.0248 mm), similarly, the centre error magnitude of the proposed algorithm (0.00512 mm) is less than 0.00553 mm. Comparing the MZC error and magnitude of the eccentricity, the proposed algorithm provides a better result. Generally, the proposed algorithm exhibits good performance with the comparison methods, as well as when using three instead of four candidate points, which provides more flexibility for detecting the optimum centre while enhancing the accuracy.

5. Conclusion

In this study, an improved minimum zone of the roundness error evaluation algorithm was developed using the alternating exchange method. The constructed minimum zone fitting function uses three candidate points to determine the expected centre coordinate, mean circle radius, and corresponding zone half-width. The initial solution was defined by applying an alternating exchange rule. The best solution function is constructed to obtain the optimal solution using the control points related to the initial solution. The validation results show that the proposed algorithm is accurate and guarantees a better approximation for the overall MZC of roundness error evaluation parameters. The use of three points provides more flexibility for detecting the optimum centre and allows the algorithm to run over the inadequacy of using the collinear candidate points in four selected points. Thus, this method improves the accuracy of the roundness evaluation of circular-shaped parts, such as the bearing ring. The effects of eccentricity and radius of components for roundness measurement accuracy will be discussed in future works.

Data availability statement

The data that support the findings of this study are openly available at the following URL/DOI: <http://dx.doi.org/10.1088/1757-899X/490/6/062052>.

Funding

This research was funded by the National Natural Science Foundation of China, Grant No. 51875166.

Conflict of interest

The authors declare no conflict of interest.

ORCID iDs

Alhadi Khilil  <https://orcid.org/0000-0001-9273-9109>

Abubakar Umar  <https://orcid.org/0000-0002-9447-0059>

References

- [1] Sui W and Zhang D 2012 Four methods for roundness evaluation *Phys. Proc.* **24** 2159–64
- [2] Y14.5M, A A 1982 Dimensioning and tolerancing (American Society of Mechanical Engineers)

- [3] Calvo R and Gómez E 2015 Accurate evaluation of functional roundness from point coordinates *Measurement* **73** 211–25
- [4] ISO No 1101 2012 Geometrical product specifications (GPS) Geometrical tolerancing tolerances of form orientation
- [5] Sundaram A *et al* 2017 Some reviews on circularity evaluation using non-linear optimization techniques
- [6] Gosavi A and Cudney E 2012 Form errors in precision metrology: a survey of measurement techniques *Qual. Eng.* **24** 369–80
- [7] Huo L *et al* 2016 Multi-level search algorithm for roundness error evaluation by the minimum zone circle method
- [8] Srinivasu D S and Venkaiah N 2017 Minimum zone evaluation of roundness using hybrid global search approach *Int. J. Adv. Manuf. Technol.* **92** 2743–54
- [9] Wen X, Xia Q and Zhao Y 2006 An effective genetic algorithm for circularity error unified evaluation *Int. J. Mach. Tools Manuf.* **46** 1770–7
- [10] Rossi A, Antonetti M, Barloscio M and Lanzetta M 2011 Fast genetic algorithm for roundness evaluation by the minimum zone tolerance (MZT) method *Measurement* **44** 1243–52
- [11] Du C-L, Luo C-X, Han Z-T and Zhu Y-S 2014 Applying particle swarm optimization algorithm to roundness error evaluation based on minimum zone circle *Measurement* **52** 12–21
- [12] Rossi A and Lanzetta M 2013 Optimal blind sampling strategy for minimum zone roundness evaluation by metaheuristics *Precis. Eng.* **37** 241–7
- [13] Lei X, Zhang C, Xue Y and Li J 2011 Roundness error evaluation algorithm based on polar coordinate transform *Measurement* **44** 345–50
- [14] Xu B *et al* 2018 Rapid precision evaluation of roundness error in polar coordinates 2018 8th Int. Conf. on Instrumentation & Measurement, Computer, Communication and Control (IMCCC)
- [15] Li X and Liu Y 2019 A quick algorithm for evaluation of minimum zone circles from polar coordinate data *Rev. Sci. Instrum.* **90** 125114
- [16] Fei L, Guanghua X, Lin L, Qing Z and Dan L 2015 Intersecting chord method for minimum zone evaluation of roundness deviation using Cartesian coordinate data *Precis. Eng.* **42** 242–52
- [17] Huang J, Chao X, Jiang L, Yang R and Tan J 2019 Improved evaluation of minimum zone roundness by integrating bidirectional search of unequal probability and offset mechanisms *Meas. Sci. Technol.* **30** 125014
- [18] Gadelmawla E S 2010 Simple and efficient algorithms for roundness evaluation from the coordinate measurement data *Measurement* **43** 223–35
- [19] Rossi A and Lanzetta M 2013 Roundness: a closed form upper bound for the centroid to minimum zone center distance by worst-case analysis *Measurement* **46** 2251–8
- [20] Samuel G L and Shunmugam M S 2000 Evaluation of circularity from coordinate and form data using computational geometric techniques *Precis. Eng.* **24** 251–63
- [21] Muralikrishnan B and Raja J 2008 *Computational Surface and Roundness Metrology* (Berlin: Springer)
- [22] Rivlin T J 1979 Approximation by circles *Computing* **21** 93–104
- [23] Wang Y, Su Y and Wang H 2019 An algorithm for roundness evaluation of crankshaft main journal *IOP Conf. Ser.: Mater. Sci. Eng.* **490** 062052
- [24] Khilil A, Ma B and Shi Z 2019 Virtual simulation of automatic quality measurement system for tapered roller bearing based on 3D automate software *J. Phys.: Conf. Ser.* **1284** 012022
- [25] B89.3.1., A 1972 American national standards: measurement of out-of-roundness (ASME)
- [26] Chetwynd D G 1979 Roundness measurement using limacons *Precis. Eng.* **1** 137–41